# Multibody joint parameter estimation using an Augmented Extended Kalman filter 

Lorenzo Mazzanti ${ }^{1,2}$, Mathijs Vivet ${ }^{1,2}$, Daniel De Gregoriis ${ }^{1,2}$, Bart Blockmans ${ }^{2,3}$

${ }^{1}$ Siemens Digital Industries Software Simulation Division<br>Interleuvenlaan 68 B-3001, Leuven, Belgium<br>lorenzo.mazzanti@siemens.com

${ }^{2}$ KU Leuven<br>Department of Mechanical Engineering<br>Celestijnenlaan 300, B-3001, Heverlee, Belgium

${ }^{3}$ DMMS Core Lab<br>Flanders Make Belgium

## EXTENDED ABSTRACT

## 1 Introduction

In recent years, state estimation techniques based on the Augmented Kalman filter [1] have been successfully used for nonlinear structural mechanics applications [2]. This approach assumes an Ordinary Differential Equation description of the underlying model used in the estimation algorithm. An Augmented Extended Kalman filter (AEKF) applicable to Differential Algebraic Equation (DAE)-described models has been introduced in [3]. This formulations is applicable to Multibody (MB) problems, as it enforces the holonomic MB constraints throughout the estimation process via projection of the Kalman update steps onto the constraints manifold. This contribution further extends the framework developed in [3] in order to perform estimation of parameters that are related to the holonomic constraints. The necessary theoretical framework and a numerical validation case are presented in the following sections.

## 2 Theory

In this work, MB systems are described in the continuous time domain using the following set of index-2 DAEs [4]:

$$
\begin{align*}
\phi(\mathbf{q}, \mathbf{v}, \mu, \lambda, \mathbf{G}) & =\mathbf{0}  \tag{1}\\
\mathbf{G}(\mathbf{q}) \mathbf{v} & =\mathbf{0}  \tag{2}\\
\mathbf{g}(\mathbf{q}, p) & =\mathbf{0} \tag{3}
\end{align*}
$$

Where: $\mathbf{q}, \mathbf{v} \in \mathbb{R}^{n_{q}}$ constitute the set of system generalized coordinates and first derivatives; $\mu, \lambda \in \mathbb{R}^{n_{g}}$ are, respectively, the two sets of Lagrange multipliers for position level and velocity levels constraints; $\mathbf{g} \in \mathbb{R}^{n_{g}}$ is the set of holonomic algebraic constraint equations, with $\mathbf{G} \in \mathbb{R}^{n_{g} \times n_{q}}$ its Jacobian with respect to $\mathbf{q} ; \phi$ is the function that describes the equation of motion of a MB system in a condensed form; $p$ represents a parameter that influences the constraint function $\mathbf{g}$. Accurate estimation of its value is the objective of this work. To accomplish this task using an AEKF, it is common to extend the set of DAEs (1-3) with a random walk model to represent the dynamics of the unknown parameter to be estimated:

$$
\begin{equation*}
\dot{p}=0 \tag{4}
\end{equation*}
$$

The estimator used in this work is derived from the well-known AEKF formulation. The state vector is defined as $\mathbf{x}=\left[\begin{array}{lll}\mathbf{q}^{T} & \mathbf{v}^{T} & p\end{array}\right]^{T}$. Expressing the set of equations (1-4) in discrete-time as $\mathbf{f}_{\mathbf{d}}$, using $k$ as timestep index, the state-space formulation becomes:

$$
\begin{gather*}
\mathbf{f}_{\mathbf{d}}\left(\mathbf{x}_{k+1}, \mathbf{x}_{k}, \gamma_{k+1}\right)+\omega_{k+1}=\mathbf{0}  \tag{5}\\
\mathbf{y}_{k+1}=\mathbf{h}\left(\mathbf{x}_{k+1}\right)+\varepsilon_{k+1} \tag{6}
\end{gather*}
$$

where $\mathbf{y} \in \mathbb{R}^{n_{y}}$ is the measurement signal; $\mathbf{h}$ is the measurement function; $\omega$ and $\varepsilon$ are zero-mean Gaussian noises with known diagonal covariance matrices $\mathbf{Q}$ and $\mathbf{R}$ that represent, respectively, uncertainties on both the system dynamics and the measurement equation. The estimator provides an estimate of the first two statistical moments of $\mathbf{x}$ given the sequence of measurements $\left\{\mathbf{y}_{\mathbf{k}}\right\}$. The first moment is the mean value of the estimate, referred to as $\hat{\mathbf{x}}$, the second moment is the state error covariance matrix P. At each time step, the AEKF used in this work performs the following actions:

1. Prediction: via integrations of the equations of motion, and propagation of the error covariance matrix using the plant error covariance matrix $\mathbf{Q}$, the algorithm provides a predicted estimate of $\hat{\mathbf{x}}_{k+1}^{-}, \mathbf{P}_{k+1}^{-}$.
2. Correction: using the Kalman update procedure, $\hat{\mathbf{x}}, \mathbf{P}$ are corrected as to decrease the mismatch between the measurement $\mathbf{y}_{k+1}$ and the prediction $\mathbf{h}\left(\hat{\mathbf{x}}_{k+1}\right)$, taking into account the measurement noise covariance matrix $\mathbf{R}$. The end results are the corrected estimates $\hat{\mathbf{x}}_{k+1}^{+}, \mathbf{P}_{k+1}^{+}$.
3. Constraint enforcement: to ensure that the post-correction estimate is constraint-compliant, $\hat{\mathbf{x}}_{k+1}^{+}$is projected onto the holonomic constraint manifold by solving the following constrained optimization problem:

$$
\begin{equation*}
\min _{\tilde{\mathbf{x}}_{k+1}}\left(\tilde{\mathbf{x}}_{k+1}-\hat{\mathbf{x}}_{k+1}^{+}\right)^{T}\left(\tilde{\mathbf{x}}_{k+1}-\hat{\mathbf{x}}_{k+1}^{+}\right) \quad \text { s.t. } \quad \mathbf{g}\left(\tilde{\mathbf{x}}_{\mathbf{k}+\mathbf{1}}\right)=\mathbf{0} \tag{7}
\end{equation*}
$$

Repeating these actions at each timestep, the end result is a sequence of estimates $\left\{\tilde{\mathbf{x}}_{k}\right\}$ that is compliant with the set of constraints applied to the MB system.


Figure 1: Visualization of the system used in the numerical validation.


Figure 2: Estimation results of the validation.

## 3 Numerical Validation

The methodology has been validated with a virtual experiment. The MB system under exam consists of a rigid pendulum connected via revolute joint to the ground. The rotational axis of this joint is at an angle of $5^{\circ}$ with respect to the world frame's $z$-axis. A visualization is provided in Figure 1. This system is used as reference to obtain position measurements that are going to be used in the estimator. White noise is added to the signal. The estimator uses a system that is equal to the reference one, but whose plane of rotation corresponds to the $x y$ plane. The objective of the AEKF is the accurate estimation of the misalignment angle $p$. The results are visible in Figure 2: both the misalignment angle and the position of the pendulum are correctly estimated.

## 4 Conclusions

In this work, an AEKF formulation suitable for MB problems has been extended for the purposes of joint parameter estimation, and validated with a numerical experiment in which the rotational axis of a revolute joint has been corrected starting from noisy measurements coming from a reference system.

## Acknowledgments

The authors gratefully acknowledge the support and contribution of the European Commission with Marie Sklodowska Curie program through the ETN ECO DRIVE project n. GA 858018. This work is supported by European Union's Horizon 2020 research and innovation programme under grant agreement No 851245 , project INNTERESTING. This research was partially supported by the VLAIO-funded project (HBC.2019.2323) "BE QUIET".

## References

[1] D. Simon, "Optimal state estimation: Kalman, $H_{\infty}$, and nonlinear approaches", John Wiley \& Sons, 2006
[2] E. Risaliti, T. Tamarozzi, M. Vermaut, B. Cornelis, W. Desmet, "Multibody model based estimation of multiple loads and strain field on a vehicle suspension system", Mechanical Systems and Signal Processing (2019), vol. 123, 1-25.
[3] T. Tamarozzi, P. Jiránek, D. De Gregoriis, (2022, July 31 - August 5) "Robust State-Input Estimation for Differential Algebraic Equations and Application to Multibody Systems", $15^{\text {th }}$ World Congress on Computational Mechanics \& $8^{\text {th }}$ Asian-Pacific Congress on Computational Mechanics 2022, Yokohama, Japan.
[4] C. W. Gear, B. Leimkuhler, G. K. Gupta, "Automatic integration of euler-lagrange equations with constraints", Journal of Computational and Applied Mathematics 12 (1985) 77-90

